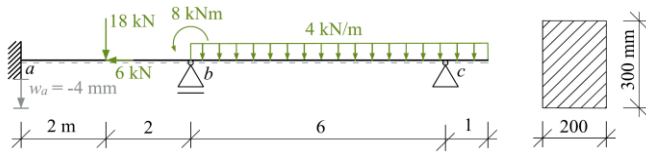


Na zadané prutové konstrukci pomocí obecné deformační metody vykreslete průběhy vnitřních sil.



1)

Výpočtový model, n_p

$$E = 24 \text{ GPa}$$

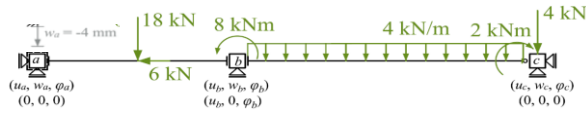
$$I = \frac{1}{12} \cdot 0,2 \cdot 0,3^3 \rightarrow$$

$$I = 4,5 \cdot 10^{-4} \text{ m}^4$$

$$EI = 10,8 \cdot 10^6 \text{ Nm}^2$$

$$EA = 1\,440 \cdot 10^6 \text{ N}$$

$$n_p = 2$$



jednotky: [m, rad, kN, kPa]

{r}

u_b
ϕ_b

{S}

0	X_b
8	M_b

Analýza prutů -- PRIMÁRNÍ ÚČINNÍKY

Prut a-b

gamma	0 [rad]	0 [deg]
sin gamma	0.00	
cos gamma	1.00	
b	0.20 [m]	
h	0.30 [m]	
delka	4 [m]	
E	2.40E+07 [kPa]	
A	0.06 [m2]	
I	4.50E-04 [m4]	
EA	1.44E+06 [kPa*m2]	
EI	1.08E+04 [kPa*m4]	

[T_ab]	1.00	0.00	0	0	0	0
	0.00	1.00	0	0	0	0
	0	0	1	0	0	0
	0	0	0	1.00	0.00	0
	0	0	0	0.00	1.00	0
	0	0	0	0	0	1

[T_ab]^T	1.00	0.00	0	0	0	0
	0.00	1.00	0	0	0	0
	0	0	1	0	0	0
	0	0	0	1.00	0.00	0
	0	0	0	0.00	1.00	0
	0	0	0	0	0	1

a) vetknuti-vetknuti

[k_ab]*	u_ab	w_ab	phi_ab	u_ba	w_ba	phi_ba	X_ab	Z_ab	M_ab	X_ba	Z_ba	M_ba
	3.60E+05	0.00E+00	0.00E+00	-3.60E+05	0.00E+00	0.00E+00	3.00	-9.00	9.00	3.00	-9.00	9.00
	0.00E+00	2.02E+03	-4.05E+03	0.00E+00	-2.02E+03	-4.05E+03	9.00	17.00	0.00	9.00	-9.50	0.00
	0.00E+00	-4.05E+03	1.08E+04	0.00E+00	4.05E+03	5.40E+03	0.00	0.00	0.00	0.00	0.00	0.00
	-3.60E+05	0.00E+00	0.00E+00	3.60E+05	0.00E+00	0.00E+00	0.00	0.00	0.00	0.00	0.00	0.00
	0.00E+00	-2.02E+03	4.05E+03	0.00E+00	2.02E+03	4.05E+03	0.00	0.00	0.00	0.00	0.00	0.00
	0.00E+00	-4.05E+03	5.40E+03	0.00E+00	4.05E+03	1.08E+04	0.00	0.00	0.00	0.00	0.00	0.00

[k_ab]	u_ab	w_ab	phi_ab	u_ba	w_ba	phi_ba	X_ab	Z_ab	M_ab	X_ba	Z_ba	M_ba
	3.60E+05	0.00E+00	0.00E+00	-3.60E+05	0.00E+00	0.00E+00	3.00	-9.00	9.00	3.00	-9.00	9.00
	0.00E+00	2.03E+03	-4.05E+03	0.00E+00	-2.03E+03	-4.05E+03	9.00	17.00	0.00	9.00	-9.50	0.00
	0.00E+00	-4.05E+03	1.08E+04	0.00E+00	4.05E+03	5.40E+03	0.00	0.00	0.00	0.00	0.00	0.00
	-3.60E+05	0.00E+00	0.00E+00	3.60E+05	0.00E+00	0.00E+00	0.00	0.00	0.00	0.00	0.00	0.00
	0.00E+00	-2.03E+03	4.05E+03	0.00E+00	2.03E+03	4.05E+03	0.00	0.00	0.00	0.00	0.00	0.00
	0.00E+00	-4.05E+03	5.40E+03	0.00E+00	4.05E+03	1.08E+04	0.00	0.00	0.00	0.00	0.00	0.00

Fx	n	M	t0
Fz	q		t1/h
a		a	alpha_t
b		b	EA
I		I	EI
-6	0	0	0
18	0		0
2		0	0
2		0	1.44E+06
4	4	4	1.08E+04

{Rp_ab}*	3.00	0.00	0.00	0.00	3.00	X_ab
	-9.00	0.00	0.00	0.00	-9.00	Z_ab
	9.00	0.00	0.00	0.00	9.00	M_ab
	3.00	0.00	0.00	0.00	3.00	X_ba
	-9.00	0.00	0.00	0.00	-9.00	Z_ba
	-9.00	0.00	0.00	0.00	-9.00	M_ba

{Rp_ab}	3.00	X_ab
	-9.00	Z_ab
	9.00	M_ab
	3.00	X_ba
	-9.00	Z_ba
	-9.00	M_ba

{r_pop}	0	u_ab
	-4.00E-03	w_ab
	0	phi_ab
	0	u_ba
	0	w_ba
	0	phi_ba

{Rpop_ab}	0.00	X_ab
	-8.10	Z_ab
	16.20	M_ab
	0.00	X_ba
	8.10	Z_ba
	16.20	M_ba

Prut b-c

gamma	0 [rad]	0 [deg]
sin gamma	0.00	
cos gamma	1.00	
b	0.20 [m]	
h	0.30 [m]	
delka	6 [m]	
E	2.40E+07 [kPa]	
A	0.06 [m2]	
I	4.50E-04 [m4]	
EA	1.44E+06 [kPa*m2]	
EI	1.08E+04 [kPa*m4]	

[T_bc]	1.00	0.00	0	0	0	0
	0.00	1.00	0	0	0	0
	0	0	1	0	0	0
	0	0	0	1.00	0.00	0
	0	0	0	0.00	1.00	0
	0	0	0	0	0	1

[T_bc]^T	1.00	0.00	0	0	0	0
	0.00	1.00	0	0	0	0
	0	0	1	0	0	0
	0	0	0	1.00	0.00	0
	0	0	0	0.00	1.00	0
	0	0	0	0	0	1

b) vetknuti-kloub

[k_bc]*	u_bc	w_bc	phi_bc	u_cb	w_cb	phi_cb	X_bc	Z_bc	M_bc	X_cb	Z_cb	M_cb
	2.40E+05	0.00E+00	0.00E+00	-2.40E+05	0.00E+00	0.00E+00	0.00	-14.50	17.00	0.00	-9.50	0.00
	0.00E+00	1.50E+02	-9.00E+02	0.00E+00	-1.50E+02	0.00E+00	0.00	17.00	0.00	0.00	0.00	0.00
	0.00E+00	-9.00E+02	5.40E+03	0.00E+00	9.00E+02	0.00E+00	0.00	0.00	0.00	0.00	0.00	0.00
	-2.40E+05	0.00E+00	0.00E+00	2.40E+05	0.00E+00	0.00E+00	0.00	0.00	0.00	0.00	0.00	0.00
	0.00E+00	-1.50E+02	9.00E+02	0.00E+00	1.50E+02	0.00E+00	0.00	0.00	0.00	0.00	0.00	0.00
	0.00E+00	-9.00E+02	5.40E+03	0.00E+00	9.00E+02	0.00E+00	0.00	0.00	0.00	0.00	0.00	0.00

[k_bc]	u_bc	w_bc	phi_bc	u_cb	w_cb	phi_cb	X_bc	Z_bc	M_bc	X_cb	Z_cb	M_cb
	2.40E+05	0.00E+00	0.00E+00	-2.40E+05	0.00E+00	0.00E+00	0.00	-14.50	17.00	0.00	-9.50	0.00
	0.00E+00	1.50E+02	-9.00E+02	0.00E+00	-1.50E+02	0.00E+00	0.00	17.00	0.00	0.00	0.00	0.00
	0.00E+00	-9.00E+02	5.40E+03	0.00E+00	9.00E+02	0.00E+00	0.00	0.00	0.00	0.00	0.00	0.00
	-2.40E+05	0.00E+00	0.00E+00	2.40E+05	0.00E+00	0.00E+00	0.00	0.00	0.00	0.00	0.00	0.00
	0.00E+00	-1.50E+02	9.00E+02	0.00E+00	1.50E+02	0.00E+00	0.00	0.00	0.00	0.00	0.00	0.00
	0.00E+00	-9.00E+02	5.40E+03	0.00E+00	9.00E+02	0.00E+00	0.00	0.00	0.00	0.00	0.00	0.00

Fx	n	M	t0
Fz	q		t1/h
a		a	alpha_t
b		b	EA
I		I	EI
0	0	-2	0
0	4		0
0		6	0
0		0	1.44E+06
6	6	6	1.08E+04

{Rp_bc}*	0.00	0.00	0.00	0.00	0.00	X_bc
	0.00	-15.00	0.50	0.00	-14.50	Z_bc
	0.00	18.00	-1.00	0.00	17.00	M_bc
	0.00	0.00	0.00	0.00	0.00	X_cb
	0.00	-9.00	-0.50	0.00	-9.50	Z_cb
	0.00	0.00	0.00	0.00	0.00	M_cb

{Rp_bc}	0.00	X_bc
	-14.50	Z_bc
	17.00	M_bc
	0.00	X_cb
	-9.50	Z_cb
	0.00	M_cb

{r_pop}	0	u_bc
	0	w_bc
	0	phi_bc
	0	u_cb
	0	w_cb
	0	phi_cb

{Rpop_bc}	0.00	X_bc
	0.00	Z_bc
	0.00	M_bc
	0.00	X_cb
	0.00	Z_cb
	0.00	M_cb

Soustava rovnic

	u_b	ϕ_{i_b}	
[K]	6.00E+05	0.00E+00	X_b
	0.00E+00	1.62E+04	M_b
{Rp}	3.00		X_b
	24.20		M_b
{F}	-3.00		X_b
	-16.2		M_b
{r}	-5.00E-06		u_b [m]
	-1.00E-03		ϕ_{i_b} [rad]

$\{F\} = \{S\} - \{R\}$

$[K] \cdot \{r\} = \{F\} \rightarrow \{r\} = [K]^{-1} \cdot \{F\}$

Analýza prutů -- SEKUNDÁRNÍ ÚČINKY

Prut a-b

{r_ab}	0	u_{ab}
	-4.00E-03	w_{ab}
	0	$\phi_{i_{ab}}$
	-5.00E-06	u_{ba}
	0	w_{ba}
	-1.00E-03	$\phi_{i_{ba}}$

Prut b-c

{r_bc}	-5.00E-06	u_{bc}
	0	w_{bc}
	-1.00E-03	$\phi_{i_{bc}}$
	0	u_{cb}
	0	w_{cb}
	0	$\phi_{i_{cb}}$

{Rs_ab}	1.80	X_{ab}
	-4.05	Z_{ab}
	10.80	M_{ab}
	-1.80	X_{ba}
	4.05	Z_{ba}
	5.40	M_{ba}

{Rs_ab}*	1.80	X_{ab}
	-4.05	Z_{ab}
	10.80	M_{ab}
	-1.80	X_{ba}
	4.05	Z_{ba}
	5.40	M_{ba}

{Rs_bc}	-1.20	X_{bc}
	0.90	Z_{bc}
	-5.40	M_{bc}
	1.20	X_{cb}
	-0.90	Z_{cb}
	0.00	M_{cb}

{Rs_bc}*	-1.20	X_{bc}
	0.90	Z_{bc}
	-5.40	M_{bc}
	1.20	X_{cb}
	-0.90	Z_{cb}
	0.00	M_{cb}

CELKOVÉ ÚČINKY

{R_ab}	4.80	X_{ab}
	-13.05	Z_{ab}
	19.80	M_{ab}
	1.20	X_{ba}
	-4.95	Z_{ba}
	-3.60	M_{ba}

{R_ab}*	4.80	X_{ab}
	-13.05	Z_{ab}
	19.80	M_{ab}
	1.20	X_{ba}
	-4.95	Z_{ba}
	-3.60	M_{ba}

CELKOVÉ ÚČINKY

{R_bc}	-1.20	X_{bc}
	-13.60	Z_{bc}
	11.60	M_{bc}
	1.20	X_{cb}
	-10.40	Z_{cb}
	0.00	M_{cb}

{R_bc}*	-1.20	X_{bc}
	-13.60	Z_{bc}
	11.60	M_{bc}
	1.20	X_{cb}
	-10.40	Z_{cb}
	0.00	M_{cb}

