

BD004

Structural Analysis 2

Lecturer: Assoc. Prof. Ing. David Lehký, Ph.D.
Institute of Structural Mechanics

Office: C 417

e-mail: lehky.d@fce.vutbr.cz

BD004 – Structural Analysis 2

Main topics:

- Moving loads and influence lines of **statically indeterminate beams**, load combinations on continuous beam.
- **The slope deflection method** (displacement method) for analysis of **indeterminate structures**
 - Principle of the method, numerical model, degree of kinematic indeterminacy
 - Analyses of simple beams, continuous beams, frames and trusses.
 - Temperature loading, support settlement, beam with variable cross section.

BD004 – Structural Analysis 2

Course organization:

- 4 hours a week =
 - 2-hour lecture (David Lehký) +
 - 2-hour exercise (Jan Eliáš)

Course completion: credit + exam

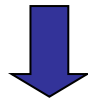
Credit – more details will provide Jan Eliáš

Exam – calculation of practical tasks + theoretical questions,
– 2 terms (a regular and a correction term) during
examination period at the end of the winter semester

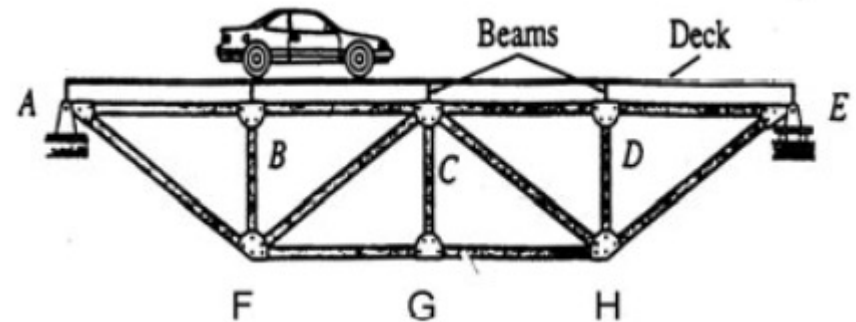
Moving loads

- Civil and bridge engineering structures (bridges, crane tracks) – **moving loads** are important (cars, trucks, trains, cranes, etc.)

Load is moving along the structure



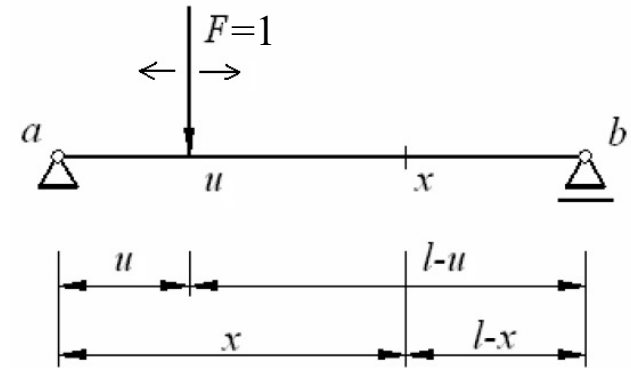
Changes of internal forces and bending moments



- In previous course (Structural Analysis 1), we have dealt with **moving loads** on **statically determinate** beams. Let's focus on **statically indeterminate** beams now.

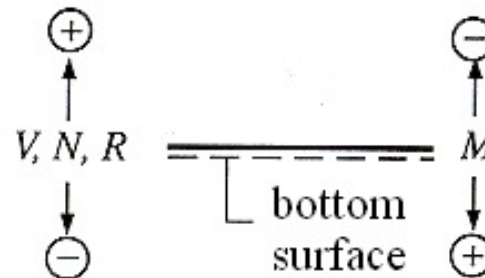
Influence lines

- Internal forces and bending moments caused by moving loads can be solved with the help of **influence lines**.
- Influence line is created using **unit load (force) $F=1$** which moves along the structure.



Influence line S_x graphs the variation of a quantity **S** at a specific point **x** on a beam or truss caused by a unit load **$F=1$** placed at any point **u** along the structure.

Signs:



Influence lines

Methods for constructing the influence line:

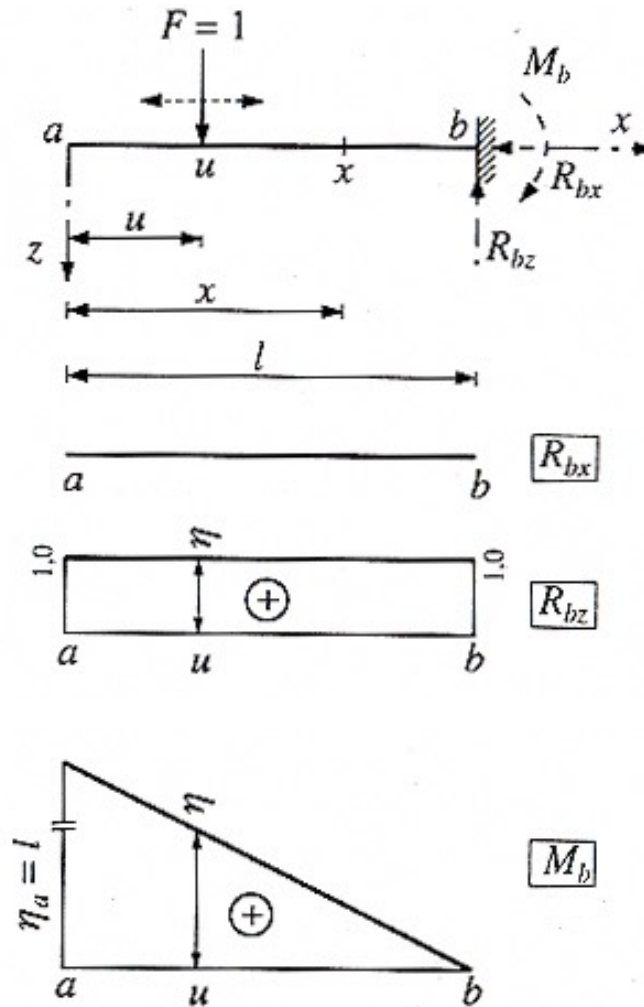
- **Analytical method** (creating equations using equilibrium conditions)
- **Kinematic method** (Müller-Breslau Principle; using principal of virtual work)
- **Combination of above-mentioned methods**

Müller-Breslau principle – The influence line for a force (or moment) response function is given by the **deflected shape** of the **released structure** obtained by **removing the restraint** corresponding to the response function and by giving the released structure a **unit displacement (or rotation)** at the location and in the direction of the response function, so that **only the response function and the unit load perform external work**.

Influence lines

Reminder: Cantilever beam – Müller-Breslau principle

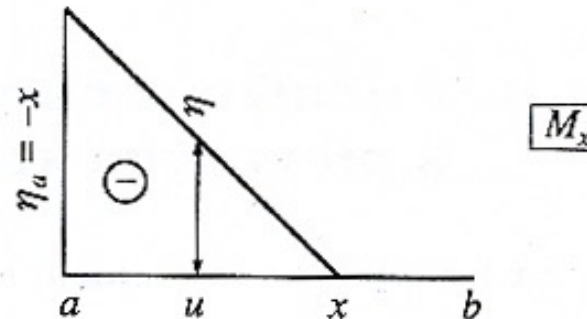
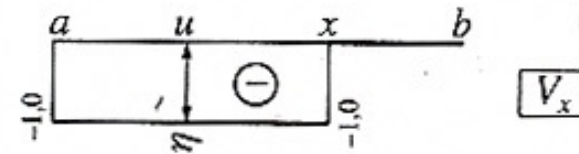
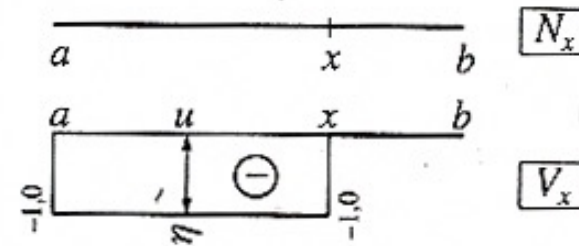
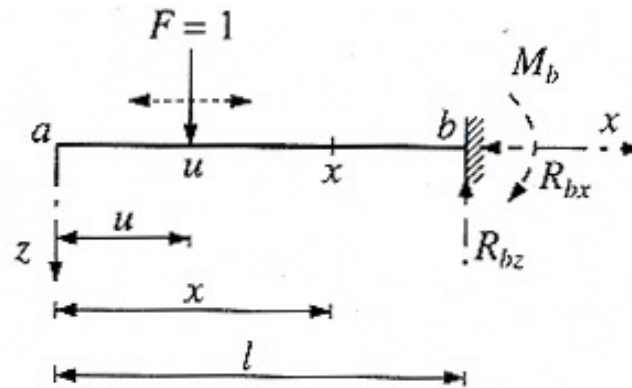
Reactions:



Influence lines

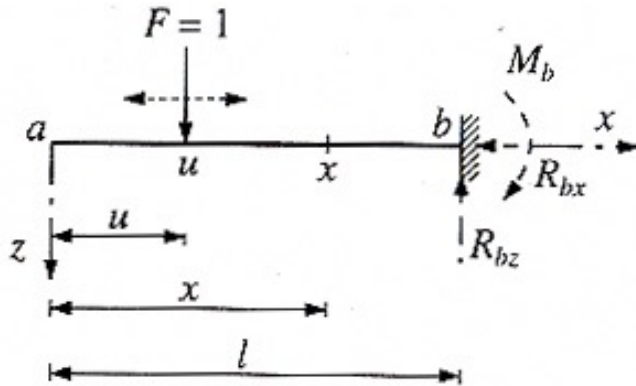
Reminder: Cantilever beam – Müller-Breslau principle

Internal forces:



Influence lines

Reminder: Cantilever beam – analytical method



$$R_{bz}$$

Equilibrium of vertical forces:

$$\sum F_{iz} = 0: 1 - R_{bz} = 0 \rightarrow R_{bz} = \eta = 1$$

$$M_b$$

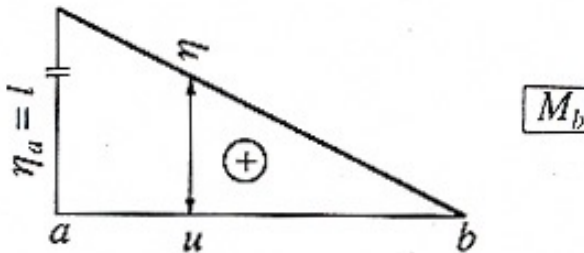
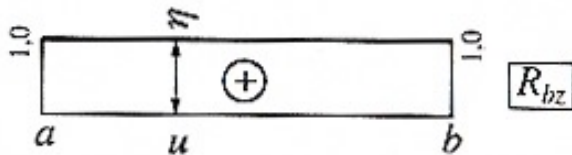
Moment equilibrium to b :

$$\sum M_{ib} = 0: 1 \cdot u' - M_b = 0 \rightarrow M_b = \eta = u' = l - u$$

Boundary conditions:

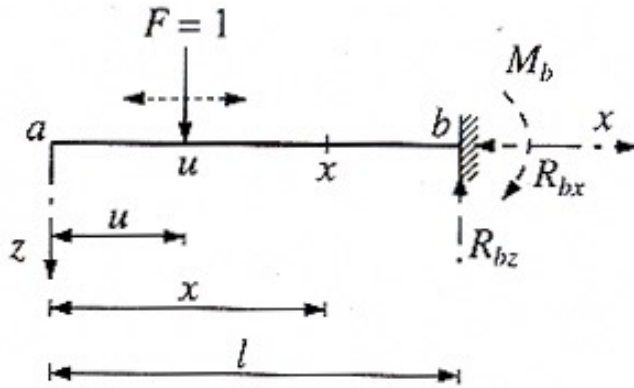
$$u = 0 : \eta = l$$

$$u = l : \eta = 0$$



Influence lines

Reminder: Cantilever beam – analytical method



$$V_x$$

Unit force is in the interval $0 \leq u < x$:

$$V_x = \eta = -1$$

Unit force is in the interval $x < u \leq l$:

$$V_x = \eta = 0$$

$$M_x$$

Unit force is in the interval $0 \leq u \leq x$:

$$M_x = \eta = -1 \cdot (x - u) = u - x$$

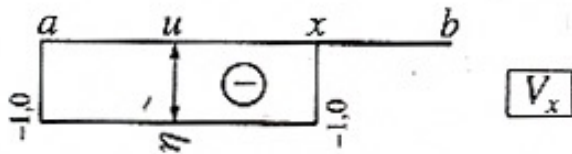
Boundary conditions:

$$u = 0 : \eta = -x$$

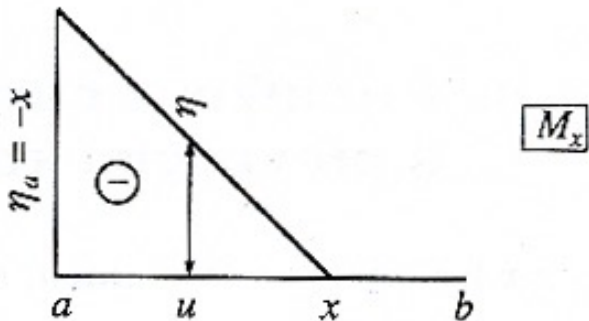
$$u = x : \eta = 0$$

Unit force is in the interval $x \leq u \leq l$:

$$M_x = \eta = 0$$



$$V_x$$



$$M_x$$

Influence lines

Statically indeterminate beam fixed at both ends – analytical method

M_a, M_b

Moments M_a, M_b using force method:

$$\Phi_{ab} = 0 : M_a \alpha_{ab} + M_b \beta_{ab} + \varphi_{ab} = 0$$

$$\Phi_{ba} = 0 : M_a \beta_{ba} + M_b \alpha_{ba} + \varphi_{ba} = 0$$

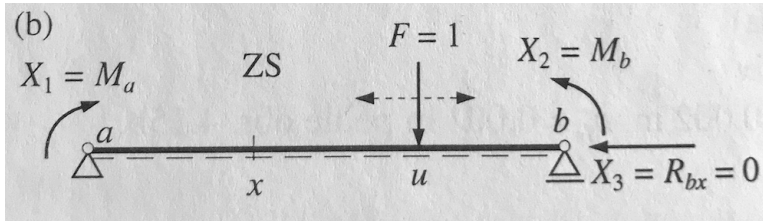
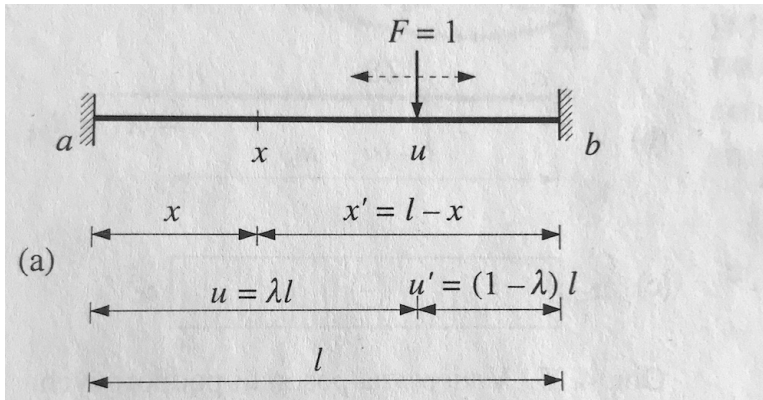
For constant cross-section:

$$\alpha_{ab} = \alpha_{ba} = \alpha = \frac{l}{3EI}$$

$$\beta_{ab} = \beta_{ba} = \beta = \frac{\alpha}{2} = \frac{l}{6EI}$$

$$M_a = -\frac{2EI}{l} (2\varphi_{ab} - \varphi_{ba})$$

$$M_b = -\frac{2EI}{l} (2\varphi_{ba} - \varphi_{ab})$$



From tables: $\varphi_{ab}^{F=1} = \frac{1 \cdot uu'}{6EI l} (l + u')$, $\varphi_{ba}^{F=1} = \frac{1 \cdot uu'}{6EI l} (l + u)$

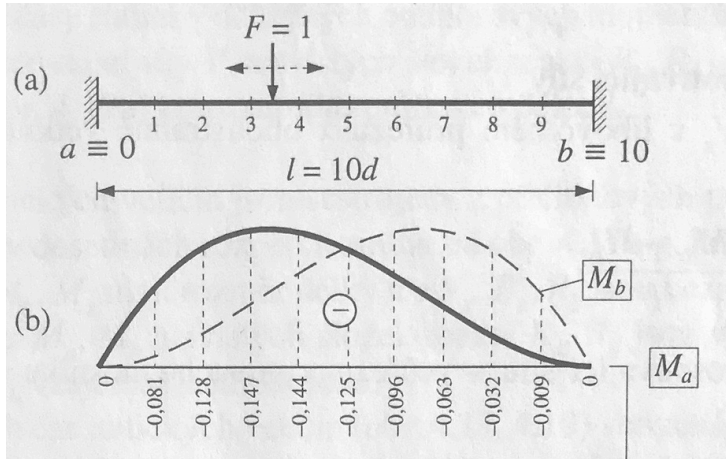
$$M_a = \eta = -\frac{uu'^2}{l^2} = -\frac{u(l-u)^2}{l^2}$$

$$M_b = \eta = -\frac{u^2u'}{l^2} = -\frac{u^2(l-u)}{l^2}$$

Cubic parabola!

Influence lines

Statically indeterminate beam fixed at both ends – analytical method



Selected ordinates:

$$\eta\left(\frac{l}{2}\right) = -\frac{\frac{l}{2}\left(l-\frac{l}{2}\right)^2}{l^2} = -\frac{\frac{l}{2} \cdot \frac{l^2}{4}}{l^2} = -\frac{l}{8} = -0,125l$$

$$\eta_{max,min}: M_a = -\frac{u(l-u)^2}{l^2} = \frac{-ul^2 + 2u^2l - u^3}{l^2} =$$

$$= -u + \frac{2u^2}{l} - \frac{u^3}{l^2}$$

$$\frac{dM_a}{du} = -1 + \frac{4}{l}u - \frac{3}{l^2}u^2 = 0$$

$$u_{1,2} = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a} = \frac{-\frac{4}{l} \pm \sqrt{\frac{16}{l^2} - \frac{12}{l^2}}}{-\frac{6}{l^2}}$$

$$u_1 = \frac{-\frac{2}{l}}{-\frac{6}{l^2}} = \frac{l}{3} \rightarrow \eta_{min} = -\frac{\frac{l}{3}\left(l-\frac{l}{3}\right)^2}{l^2} = -\frac{4}{27}l = -0,148l$$

$$u_2 = \frac{-\frac{6}{l}}{-\frac{6}{l^2}} = l \rightarrow \eta_{max} = 0$$